In the Specification

Kindly replace paragraph [0008] with the following:

[0008] However, it has been known that when a high-strength steel sheet having a tensile strength of 440 MPa or more or a higher tensile strength of 500 MPa or more or 590 MPa or more is produced by the technique of adding solid-solution strengthening elements to ultra low carbon steel used as a raw material, the amounts of the alloy elements added are increased to cause the problem of surface appearance, the problem of degrading plating performance, the problem of secondary cold-work embrittlement, and the like. Also, the addition of large amounts of solid-solution strengthening elements decreases the r value, thereby causing the problem that the r value level is decreased as strength is increased. Furthermore, in order to decrease a carbon content to the ultra low carbon region, such a C content of less than 0.010% as disclosed in the ~~cited document 1~~ Japanese Unexamined Patent Application Publication No. 56-139654, vacuum degassing must be performed in a steel making process. This means that a large amount of CO_2 is generated in a production process. Therefore, from the viewpoint of global environment conservation, it is difficult to say that this technique is a preferable technique.

Kindly replace paragraph [0021] with the following:

[0021] A texture suitable for deep drawability is developed under a condition in which unlike in conventional ultra low carbon IF steel, the amount of dissolved C adversely affecting deep drawability is not excessively decreased in a ~~rage~~ range of 0.010 to 0.050% by mass, leaving an amount of dissolved C necessary for forming a martensite phase, thereby securing an average r value of 1.2 or more and high drawability and forming a dual-phase microstructure of steel having a ferrite phase and a second phase including a martensite phase. As a result, a high

strength TS of 440 MPa or more, preferably 500 MPa or more, and more preferably 590 MPa or more can be achieved.

Kindly replace paragraph [0038] with the following:

C: 0.010 to 0.050%

[0038] C is an important element ~~for the present invention~~ together with Nb which will be described below. C is effective in increasing strength and promotes the formation of a dual phase containing a ferrite phase as a matrix phase and a second phase including a martensite phase. With a C content of less than 0.010%, the formation of the martensite phase becomes difficult. ~~In the present invention, therefore~~ Therefore, 0.010% or more, preferably 0.015% or more, of C must be added from the viewpoint of formation of a dual-phase. In particular, in order to obtain a high strength TS of 500 MPa or more, of course, the strength can be adjusted using solid-solution strengthening elements, such as Si, Mn, P, and the like, in addition to the formation of a dual phase. However, from the viewpoint of making use of the characteristics of the steel sheet ~~of the present invention~~, which is a dual-phase steel sheet, the strength is most preferably adjusted by controlling the C content. In this case, the C content is preferably controlled to 0.020% or more, and in order to obtain a TS of 590 MPa or more, the C content is preferably controlled to 0.025% or more. Also, the C content preferably satisfies the relation to Nb, (Nb/93)/(C/12) = 0.2 to 0.7, and more preferably the relation, (Nb/93)/(C/12) = 0.2 to 0.5.

Kindly replace paragraph [0045] with the following:

Al: 0.005 to 0.5%

[0045] Al is useful as a solid solution strengthening element and a deoxidization element for steel, and has the function to fix solute N present as an impurity to improve the anti-aging property. Furthermore, Al is useful as a ferrite forming element and a temperature control

element for a α-γ intercritical region. In order to exhibit the function, the Al content must be 0.005% or more. On the other hand, the Al content exceeding 0.5% causes a high alloy cost and induces [[a]] surface ~~defect~~ defects. Therefore, the upper limit of the Al content is 0.5% and preferably 0.1% or less.

Kindly replace paragraph [0092] with the following:

[0092] Although details are not clear, therefore, it is supposed that an inclination of 5° or more is effective in promoting the occurrence of a recrystallization nucleus suitable for deep drawability from a grain boundary ~~in the present invention~~.

Kindly replace paragraph [0102] with the following:

[0102] The hot-rolled sheet is preferably pickled for removing scales before cold rolling. The pickling may be performed under ordinary conditions. The cold rolling conditions are not particularly limited as long as the cold-rolled sheet having desired dimensions can be formed. However, the reduction rate of cold rolling is preferably at least 40% or more, and more preferably 50% or more. A high reduction rate of cold rolling is effective in increasing the r value. When the reduction rate is less than 40%, the {111} recrystallized texture is not easily developed, and thus excellent deep drawability is difficult to achieve. On the other hand, ~~in the present invention,~~ the r value is more increased as the reduction rate of cold rolling is increased in a range of up to 90%. However, when the reduction rate exceeds 90%, the effect is saturated, and the load on a roll in cold rolling is increased. Therefore, the upper limit of the reduction rate is preferably 90%.